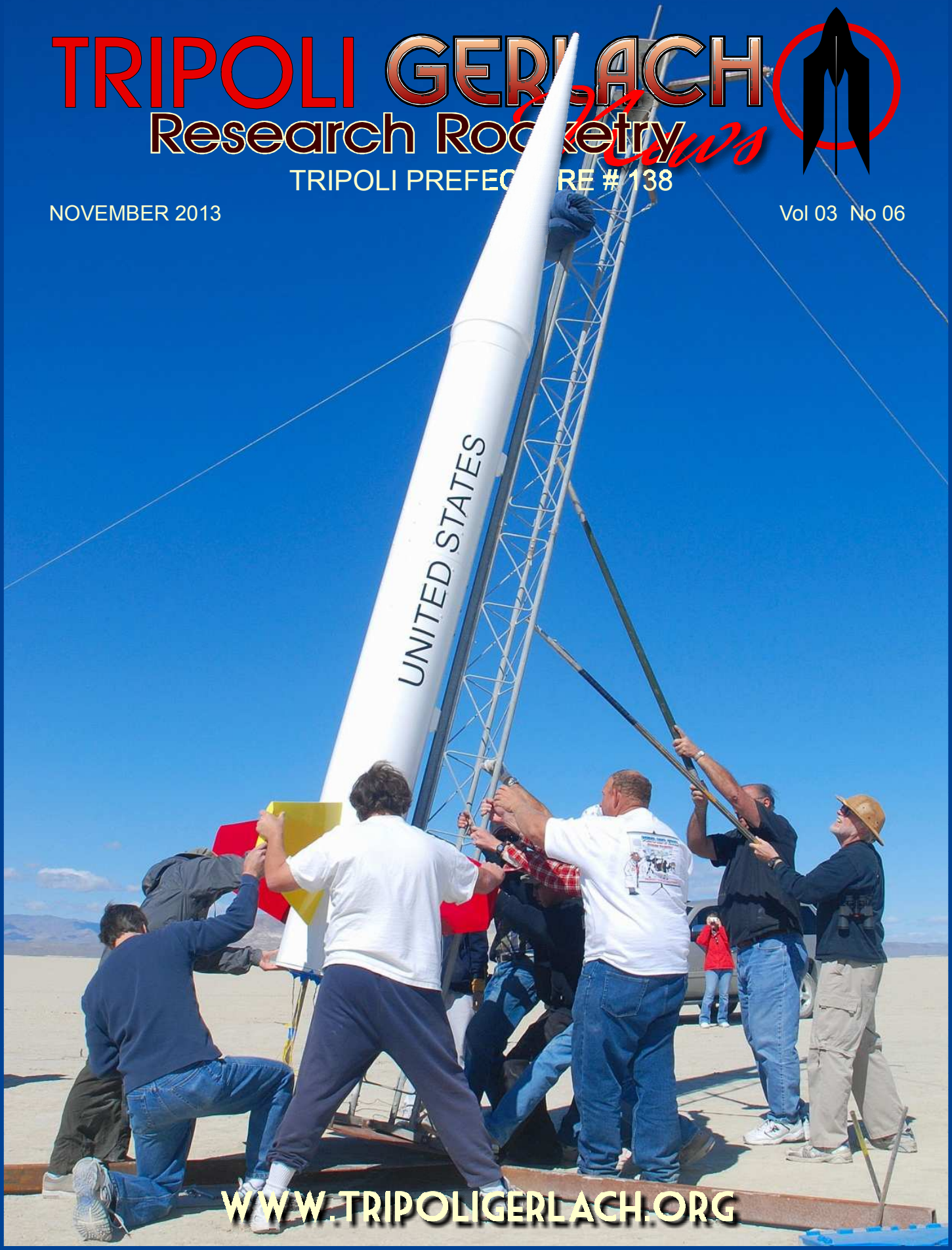
TRIPOLI GERLACH Research Rocketry News

TRIPOLI PREFECTURE # 138

NOVEMBER 2013

Vol 03 No 06



WWW.TRIPOLIGERLACH.ORG

TRIPOLI GERLACH Research Rocketry
TRIPOLI PREFECTURE #138

NOVEMBER 2013 Vol. 03 No. 06

PUBLISHED EXCLUSIVELY FOR
THE MEMBERS OF TRIPOLI GERLACH
AND ANYONE ELSE INTERESTED

Tripoli Gerlach was founded as a National Prefecture under the Tripoli Rocketry Association, Inc. Devoted to Research Rocketry and the Black Rock Desert area of Nevada, we welcome all National Tripoli Members, no matter their location or Certification Level.

Our Executive Officers are;

Gary Rosenfield (022)
Prefect
Cedar City, UT
garoq@scinternet.net

Tom Blazanin (003)
Secretary
Valencia, PA
shadow@pghmail.com

Dave Rose (7126)
Treasurer
N. Huntingdon, PA
drose191@comcast.net

If you have anything to contribute in the way of information, articles, photos or whatever, please send them to Tripoli Gerlach Headquarters. Visit our WebSite on-line at;

WWW.TRIPOLIGERLACH.ORG

ON THE COVER Jack Garibaldi, of What's Up Hobbies, and crew raise Jack's NIKE SMOKE. Black Rock proves to be the best venue for large and extremely powerful rockets whether its LDRS or BALLS. Makes you wonder what we'll see next year!

Photo by Mark Canepa

MAGAZINE STAFF

EDITOR & LAYOUT:
Tom Blazanin

CONTRIBUTING STAFF:
Chris Pearson
Gerald Muex, Jr

OFFICE:
Tripoli Gerlach
748 Galloway Drive
Valencia, PA 16059

CLOSING

This issue of *TRIPOLI GERLACH NEWS* ends our third year as a Prefecture under the Tripoli Rocketry Association, Inc.

This little E-Magazine returns a lot of positive comments from all over the place. Especially Non-Tripoli Gerlach members and Non-Tripoli members period. We hope we can continue for 2014 to bring articles of interest for both rocketry and the Black Rock area.

As a Prefecture we accomplished quite a lot putting out six issues if this on time is a start. We also held an LDRS at Black Rock. While small in size we received a lot of good words and thanks from those who attended.

Our little HAMSTER DANCE launch went off without any problems and provided some laughs and interesting flights - how's 13,030 feet sound?

Probably last and most important is we actually got Meat Balls with our Spaghetti Dinner!

Hopefully our membership will grow in 2014. Send in your renewals if you haven't already. And try to get others in your area to join us. – See you in 2014.

DISCLAIMER

Tripoli Gerlach does NOT promote nor certify any activities presented here as safe nor appropriate to all readers of this Publication. Information is for educational purposes only. Tripoli Gerlach, its members & officers, the authors of articles presented and the Tripoli Rocketry Association, Inc. are not responsible for reader's activities, conduct or participation in the use and pursuit of any content presented.

ANNUAL MEMBER'S MEETING 2013

Tripoli Gerlach is unique in that it has members from literally all over the world. It is the only Tripoli Prefecture in a town where no members live. It is also unique in that it holds but one meeting a year, that being its Annual Member's Meeting held the Friday evening of the BALLS Launch. September 20th, 2013 saw Tripoli Gerlach's third annual Member's Meeting held in the WayBack Room at Bruno's Country Club.

While not all members can attend every year we still had a really good turn out for business and a Spaghetti Dinner - with Meat Balls! In addition we picked up several new members to our ranks as reflected on our WebSite's CURRENT MEMBERS Page.

The first real order of business was to ratify a change in our By-Laws voted on earlier in the year by all of the members regarding the permitting of National Tripoli Members of any Certification Level. This was agreed upon almost unanimously by an E-Mail vote and unanimously by all members attending the meeting. The Bylaws are now officially changed and posted on our WebSite.

Next up LDRS 32 was discussed. While everyone who attended it thought it a huge success it was in fact one of the smallest modern day LDRS's. Everything ran smoothly, The banquet and give-a-ways went smoothly yet the event dropped its last day of launch activities due to the small remaining attendees. While we did not make any money on the event, as a club we didn't loose any either.

Despite the small attendance it was brought up to hold another LDRS at Black Rock in the near future, this

Gary Rosenfield assumes Tripoli Gerlach leadership taking over the position of Prefect for 2014.

time for only the standard three days. The membership in attendance all seem to be interested in pursuing this and we will discuss it further amongst small groups before we make a commitment.

HAMSTER DANCE 3 was brought up. Once again it came off as another success. Awards were passed out with Dinner Certificates going to Larry Benek (heaviest rocket), Gary Rosenfield (lightest rocket) and Bill Good (nicest rocket. Eric Cayemberg got a Dinner Certificate and captured the Alpha Hamster Award for 2013 with the highest altitude of 13,030 feet.

New Officers were place with Dave Rose as Treasurer, Tom Blazanin moved to the Secretary position and Gary Rosenfield took over as Prefect of our group.

Meeting was ended with the next Annual Meeting being set for Friday evening of BALLS 23, whenever that will be.

Members of Tripoli Gerlach enjoy a nice meeting, social gathering and spaghetti dinner - with meat balls this year. In all eight tables were used and as usual friendships were bonded. If you missed it this year make sure not to miss next year's event - it's your Prefecture.

It started out as a joke with three participants. The second year we had nine people. This year we had twelve flyers and slightly more spectators. The world of High Power is finding HAMSTER DANCE a fun and viable exercise in how good can you make a motor…

L to R - Ken Finwell, Bill Good Sr, Ken Good, Gary Dickinson, Larry Benek, Dave Rose, Gary Rosenfield, Ken Overton, Andy Limper and Bill Good. - Missing are Eric & Tom Cayemberg and Marc Stevens.

3rd Annual HAMSTER DANCE The National WENTEX Launch

'The little launch that could' is finding more and more popularity with those flyers and motor makers that want to have fun again with rockets. The challenge is to build and successfully fly a rocket with a 5 lb lift off weight using a homemade single use motor containing no metal parts in its structure.

This third event in the series went off really well with twelve participants, one taking it too serious by attaining an altitude of 13,030 feet. This will bring some new rules to the event for HAMSTER DANCE IV in 2014.

Holding with the tradition of seeing more of the Black Rock Desert this year's event was held at Smoke Creek, a dry lake Southeast of Gerlach. The very same site used by the RRI in the early pre-Tripoli days of Experimental Rocketry. Flyer Gary Rosenfield and spectators Chuck and Clare Piper were the only persons attending to claim rites of previous activities at this site back in those good old days.

The area still held Rocket Fossils of those long gone days when those on the leading edge of High Power threw spit into the wind to fly Large & Dangerous Rocket Ships - to the chagrin of the NAR!

This year's HAMSTER DANCE event was far calmer and more organized then by gone days at this location yet the spirit of rocket research was in full swing.

Gary Rosenfield

Andy Limper

Larry Benek

Dave Rose

HAMSTER DANCE went as intended with an excessive amount to failures, laughs and humility. When they went good they were great - when they went wrong they were still great!

Andy Limper returned with his infamous Weenie Rocket. This time with Viagra, a long finned stabilizer stick. Must have really worked well as it had a pre-mature ejection on the pad!

Lightest Rocket went to Gary Rosenfield, 22oz, while the Heaviest Rocket, 4.33lbs went to Larry Benek. The best looking Rocket voted on by the spectators, was Bill Good with his big stock Der Red Max, Goes to show anything goes!

Eric Cayemberg took the prize with a sizzling altitude return of 13,030 feet to capture the title of ALPHA HAMSTER 2013. Of course his claim is disputed by some flyers who claim their rockets are still going up because they couldn't find them anywhere on the ground!

Overall everyone had a great time, not only flying rockets but visiting Smoke Creek, the Holy Land where it all started.

Next year's HAMSTER DANCE IV will be held on the Black Rock Playa straight out east of the 3 Mile Entrance. This will give those with no sense of humor a higher waiver and plenty more open area!!

PLAN NOW TO JOIN US!

ALPHA HAMSTER 2013
Eric Cayemberg - 13,030 feet

Tom Cayemberg

Ken Finwell

Ken Overton

Gary Dickinson

Bill Good

Bill Good Sr

Marc Stevens

STEVEN'S CAMP

Stevens Camp is a popular camping area located at the North end of High Rock Canyon. It is a convenient and accessible camping area that provides a good base camp for exploration of High Rock Canyon and the surrounding uplands - rich in game and not many people - yah sure!

To the Northwest of the Black Rock Playa lies a place called High Rock Canyon. Its an extremely scenic area of high walled rock formations, petroglyphs and a road only traversable with a 4 wheel drive vehicle. It's a hikers, bikers and rock climbers delight.

You can access High Rock Canyon by heading north on Rt 34 out of Gerlach. Pass the 12 mile Playa entrance and continue north for almost 30 miles. Turn east on a road known as Little High Rock Road to High Rock Lake. You then head North on High Rock Canyon Road.

This is known as the South Gate to High Rock Canyon. The canyon runs about 12 miles north to a location called North Gate, which is more easily accessed from Rt8A to the north heading East out the "town" of Vya.

Just north of the actual North Gate to High Rock Canyon lies Steven's Camp. A galvanized steel "house" in the middle of nowhere. This is a sanctuary for stranded travelers and hunters caught in bad winter weather. In the summer it's used by tourists exploring High Rock Canyon and the surrounding uplands. While in the middle of nowhere the cabin is full most of the summer, so don't expect to be the only person looking to use the facilities

The cabin itself is available for public use on a first-come first-served basis and includes amenities such as running water (must be treated prior to drinking), a wood stove, a shower and hot water heater, and connections for a generator to provide power and lights to the cabin.

Fresh water flows right outside the cabin. It is ice cold and refreshing. It is drinkable but many people say to boil it first (that would loose the freshness) because it is about 100 yards away from the outhouse. Hey! We're tired and hot and thirsty. None of us has died yet!

On our arrival a group had set up base for an Off-Road Bicycle Run up High Rock Canyon. They basically were the finish line and had food and drinks for the bike participants due to arrive at anytime.

Activities like this go on all the time and this cabin in the middle of nowhere is well used.

The cabin was built on BLM land without BLM permission by winter hunters primarily for winter hunters who might get stranded in the Nevada snows. It has been maintained so well by people who take advantage of its existence that the BLM has given its blessing. Even still no one officially maintains it.

The inside is not quite as bare as you would think. With a portable generator hooked up to the electreical panel there is light and a working refridgerator. There is even a connection for a propane tank and the gas stove can be used to cook.

There are several double bunk beds. Springs only, you supply the bedding, however, there are some blankets available to the stranded traveler.

There is even a supply of can goods in the cabinets, probably donations from past inhabitants. And the neatest thing is nobody abuses this facility. Use what you want, take what you need. Please replenish if and when you can.

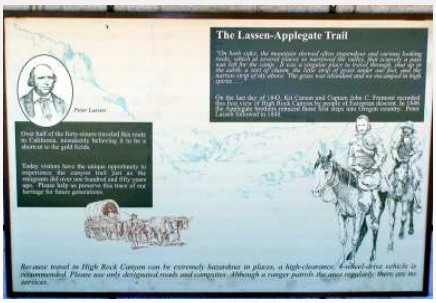
There is even a supply of wood for the wood burning stove, which is the main source of winter heat. The wood is there to use, maybe replace it before you leave.

A Visitors Book is there and the signed signatures are from all over the world.

CODE OF THE WEST
(A sign inside the door)

An 'open door' in the desert wide. . .
Invites all strangers to come inside
Build a fire and get a good nights rest
But don't forget the "Code of the West"
Leave the cabin clean and the wood piled high
For the next desert stranger who happens by.*
** it could be you.*

As with all good things that occur in life the BLM has laid claim to this facility. It was too good for them to tear down so they just absorbed it into their realm of existence. While they do not stop anyone from using it, they don't even ask for a permit, they had to stake their claim by placing bunches of educational signs all over the property. All in all it's good stuff and they mean well. Too bad there are not more places like this around the Black Rock Desert.



LOAD CELLS PRIMER

The following is derived on information from SI Technologies' Revere Transducers product line. Products listed are readily available from various easy to locate distributers. Information presented, while covering RT Transducers, is applicable as a knowledge base to nearly all Transducers on the market. Actually All You' ll Ever Need To Know About Load Cells.

The heart of any weighing system is the load cell. Whilst they are not exciting to watch, load cells are highly accurate transducers which provides the user with information not generally obtainable by other technology due to commercial factors. Load cells are designed to sense force or weight under a wide range of adverse conditions; they are not only the most essential part of an electronic weighing system, but also the most vulnerable. In order to get the most benefit from the load cell, the user must have a thorough understanding of the technology, construction and operation of this unique device. In addition, it is imperative that the user selects the correct load cell for the application and provide the necessary care for the load cell during its lifetime. Understanding these important issues and properly maintaining the load cells will ensure trouble free weighing for a long period of time.

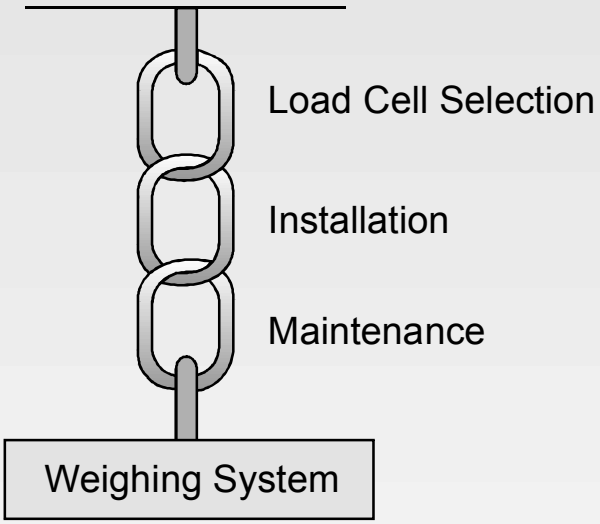


Figure 1 The most important factors for a weighing system are linked like a chain; each link requires attention for a long term success.

Load cells may be damaged because of (shock) overloading, lightning strikes or heavy surges in current, chemical or moisture ingress, mis-handling (dropping, lifting on cable, etc.), vibration, seismic events or internal component malfunctioning. This article will focus on the Do's & Don'ts for load cells as well as on basic system design.

1. LOAD CELL SELECTION

Load cell selection in the context of trouble free operation concerns itself primarily with the right capacity, accuracy class and environmental protection, rather then with a particular measuring principle like bending, shear, compression or ring torsion. While saying this, it should also be recognized that a particular measuring principle might offer distinct advantages in terms of overload capabilities or the ease of mounting. The different principles of operation will therefor be discussed shortly:

1.1 Strain gage load cells

The sensing, or spring, element is the main structural component of the load cell. The element is designed in such a way that it develops a strain, directly proportional to the load applied. Sensing elements are normally made of high strength alloy steels (nickel plated for environmental protection), precipitation - hardened stainless steels, heat treated aluminum alloys, or beryllium copper alloys.

By bonding strain gages to a precisely machined element, the force applied can be identified in terms of resistance change. The strain gages, usually four or a multiple of four, are connected into a Wheatstone bridge configuration in order to convert the very small change in resistance into a usable electrical signal. Passive components such as resistors and temperature depending wires are used to compensate and calibrate the bridge output signal.

1.1.1 Bending load cells

Sensing elements which are subjected to bending moments are widely used in many configurations for commercial transducers. Bending beams offer high strain levels at relatively low forces, which makes them ideal for low capacity load cells.

Furthermore, in case of a beam with a symmetrical cross section about the bending axis, there are always two surfaces subjected to equal strains of opposite sign. This offers convenient means for implementing a full bridge circuit, while temperature compensation is relatively

easy.

Most products using the bending principle are of the parallelogram or double bending type. Revere Transducers' single point load cell type 642 is a straight forward parallelogram, while low capacity BSP, HPS and USP use this configuration but in a mechanically more complicated manner.

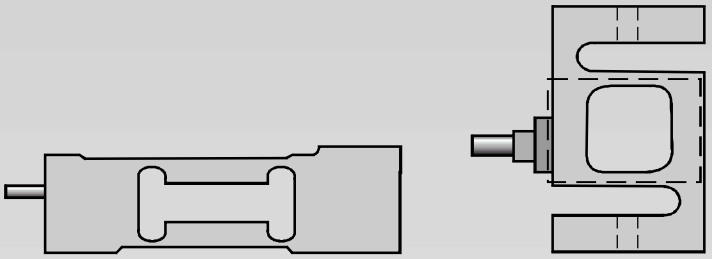


FIG 2 Load Cell Types 642 and 363

Bending as a measuring principle offers excellent linearity. Bending beams have relatively high strain levels with greater deflection compared to other measuring principles. This in turn means that although the cell is subjected to greater static overload, mechanical stops are more feasible. The dynamic overload capabilities are excellent because of the typical high deflection.

1.1.2 Shear load cells

Shear (beam) load cells have become increasingly popular for all types of medium and high capacity applications. Shear as a measuring principle offers a standard profile for a given capacity, good resistance against side loads and a relatively small sensitivity to the point of loading.

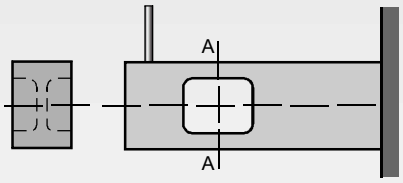


FIG 3 Principle of Shear-Web Sensing Element

At section A-A of the beam, a recess has been machined in each side, leaving a relatively thin web in the center. Just as in a structural I-beam, most of the shear force imposed by the load is carried by the web, while the bending moment is resisted primarily by the flanges. At the neutral axis, where the bending stress is negligible, the state of stress on the web is one of pure shear, acting in the vertical and horizontal directions.

As a result, the principle axis there are at 45º to the longitudinal axis of the beam, and the corresponding principal strains are of equal magnitude and opposite sign. Pairs of strain gages are installed on both sides of the web and connected in a full-bridge circuit for load measurement. Although it is more difficult to install the strain gages in some form of recess, they can readily be sealed and protected against environmental effects.

Shear-web sensing elements are not limited to beam configurations. Revere Transducers' higher capacity BSP and USP use this configuration in a more complicated manner.

Low capacity shear load cells are difficult to produce, because they require a very thin web to obtain the necessary strain levels. High capacity shear load cells are usual based on dual shear webs in a beam configuration, as single ended beams become expensive and cumbersome to mount.

Shear beam load cells are relatively insensitive to the point of loading and offer a good resistance to side loads. This simplifies its use in many weighing applications. The overload capabilities are usual slightly better compared to bending beams, although mechanical stops are less feasible because of minimal deflection.

1.1.3 Compression load cells

Compression load cells can be based on shear, bending, ring torsion or column measurement. The column load cell has a history which dates back to the earliest strain gage transducer. As indicated below, the column element consists of one (single column) or more (multiple column) members. Although conceptually simple, the column element has a number of specific characteristics which makes these load cell types difficult to design and produce. The column itself should be long enough, with respect to its cross section, to provide a uniform strain field, unaffected by end conditions. Since the column configuration is subject to second-order effects from off-axis or off-center load components, provisions must be made to minimize these, for example by using two diaphragms at the upper end of the column.

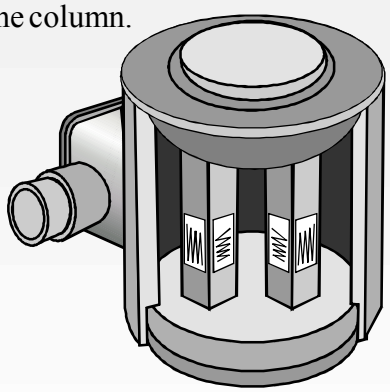


FIG 4 RT Mu;ti-Column Load Cell Type CSP

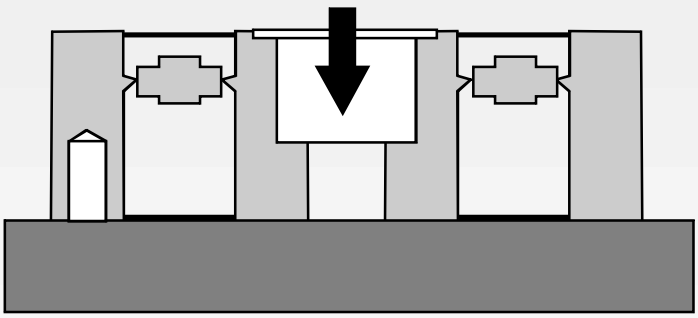
Column load cells are inherently non-linear due to the change in cross section, while deforming under load (Poisson's ratio). This non-linearity can be compensated for with semiconductor gages, connected in the plus and minus excitation lines. The output of the semiconductor gage thus serves as a feedback for adjusting the bridge voltage in the opposite direction to that of the non-linearity error.

Single column load cells become tall and difficult to handle (heavy), when designed for very high loads. Low profile canisters can be obtained if the load is carried by three or more columns, each column with its own set of gages. The corresponding gages from all of the columns are connected in series in the appropriate Wheatstone bridge arms. The result is not only an overall low profile, but also an improved performance when the cell is off-center or off-axis loaded. Compression type load cells don't suffer from the momentum typically associated with beams. The ultimate overload capabilities are therefor excellent. However, the relatively small deflection makes these load cell types more sensitive to shock loading.

1.1.4 Ring torsion load cells

The ring torsion measuring principle is relatively new, and ideally suited for the capacity ranges which are typically served by shear and bending beams. Revere Transducers load cell model RLC is a low profile, stainless steel ring torsion load cell, based on a full bridge circuit of four circular strain gauges. The strain gauges are bonded to a ring-shaped part of the element which will bend when load is introduced. This process will cause a decrease of the ring diameter at the top, while the bottom experiences a diameter increase. Hence, two gauges are compressed and two gauges are in tension, when the unit is loaded.

FIG 5 Cross Section of Load Cell Type RCL



The geometrical design of the sensing element provides enhanced specifications in terms of creep and hysteresis compared to shear and bending as a measuring principle.

Due to its compression loading mode, the unit does not suffer from the momentum typically associated with beams, and is therefore an inherently safer device, while maintaining an extremely low profile. Mechanical overload protection is established by the pre-determined distance between the load introduction ring and the base plate. Ring torsion load cells have a very low deflection, which makes them ideal for high speed weighing, but they are also more sensitive to shock overloading.

1.2 CAPACITY SELECTION

Overload is still the primary reason for load cell failure, although the process of selecting the right load cell capacity looks easy and straight forward on first sight. Capacity selection requires a fundamental understanding of the load related terms for load cells as well as the load related factors associated with systems. The load related terms for load cells are:

Load cell measuring range:
The range of values of mass for which the result of measurement should not be affected by an error exceeding the maximum permissible error.

Safe load limit:
The maximum load that can be applied without producing a permanent shift in the performance characteristics beyond those specified; specified as a percentage of the measuring range (i.e. 150%).

Ultimate overload:
The maximum load that can be applied without physical destruction of the load cell; specified as a percentage of the measuring range (i.e. 300%).

Safe side load:
The maximum load that can act 90E to the axis along which the load cell is designed to be loaded at the point of axial load application without producing a permanent shift in the performance beyond those specified; specified as a percentage of the measuring range (i.e. 100%).

Summary:
A load cell will perform within specifications until the safe load limit or safe side load limit is passed. Beyond this point, even for a very short period of time, the load cell will be permanently damaged. The load cell may physically break at the ultimate load limit.

The factors that contribute to the weight load on the load cells are: Zero tracking, initial zero setting, dead load, maximum scale capacity, location, and specific factors like wind forces or seismic events.

In addition to these, it is often necessary to derate the load cells (use a higher capacity) because of:
Shock loading
Dynamic influences (agitators)
Off centre loading to the scale
Off centre distribution of dead load
T he possibility of an overload weight

The difference between normal or static overload and shock overload is often misunderstood and needs further explanation. Static overload is defined as a gradual increase in weight over and above the rated capacity of the load cell.

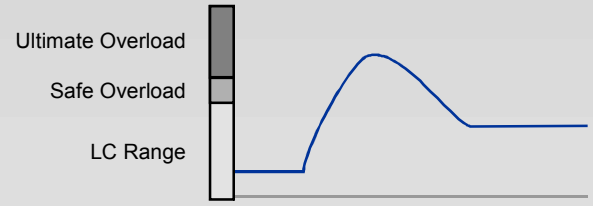


FIG 6 Static Overload

Systems can be protected by incorporating mechanical stops, or by selecting load cells with a higher capacity.

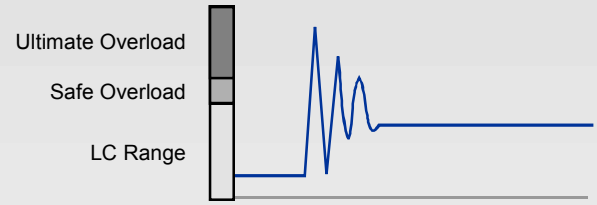


FIG 7Shock Overload

Shock overload can be defined as a sudden change in weight, within a very short period of time, over and above the rated capacity of the load cell. This situation specifically occurs when a relatively small non-elastic item is dropped from a considerable height on the scale.

Systems can be protected by incorporating shock insulation pads, or by selecting load cells with a higher rated capacity. Mechanical stops act to assist the protection against shocks. Particular care must be given to load cells with a low deflection, as they are more sensitive to dynamic overload. Both types of overload result in a sudden change of zero balance, the temperature compensation on zero is also affected. The following calculations and table should be used to calculate the correct load cell capacity:

$$Lccap = Ft+Fw +(Deadload+Liveload*Fa)/N$$

where;
N Number of load cells
Fa Dynamic load factor
Fw Effect of wind force (for hoppers)
Ft Combined effect of zero setting devices:

$$Ft = Liveload * Zero\ setting\ devices(\%) / (N*100)$$

* Determine the value based on the load cell's measuring principle (low deflection - value high).

	Fa	*De-rate**
Platform scale	*1.4*	*30-50%*
Weighbridge	*1.4*	*30-50%*
Single cell application	*1.3*	*20-40%*
Single cell hybrid bridge	*1.2*	*10-30%*
Hopper; equal load dis tribution	*1.1*	*10-30%*
Hopper; unequal load distribution	*1.2*	*20-40%*
Hopper; with agitator	*1.3*	*20-40%*

For example:
A platform scale with a capacity of 1500kg is built with four load cells. The scale has an initial zero setting of 16% and a zero tracking of 4%. The dead load equals 100kg. The load cell capacity should be:

$$Ft = 1500*(16+4) / (4*100) = 75$$

$$LCcap = [100+(1500*1.4) / 4] +75+0 = 625kg$$

Depending on the load cell's measuring principle, the required load cell capacity varies between 895 and 1250 kg (derate 30 to 50%).

It is important to verify the output per scale division with the required minimum signal level for the measuring device to ensure compatibility. The output per division (in μV) can be calculated by:

$$(UE*S*Liveload*1000) / (N*LCcap*n)$$

where:
UE Excitation voltage
S Rated output load cell
n Number of scale divisions

For example:
The presented scale configuration is built with 4 load

cells, output 2mV/V, 3000 divisions, rated capacity 1000 kg and an excitation voltage of 10V. The output per division will be:

$$(10*2*1500*1000) / (4*1000*3000) = 2.5\mu V$$

-1) ACCURACY

Load cells are ranked, according to their overall performance capabilities into differing accuracy classes. Some of these accuracy classes are related to standards which are used in legal for trade weighing instruments, while other accuracy classes are defined by the individual load cell manufacturer. Depending on the standard and the performance of a particular load cell type, an alphanumeric "accuracy grade" is given to the product. The alpha designate refers to the specific accuracy class, while the numeric part refers to the number of divisions.

Revere Transducers manufactures products meeting NTEP, OIML and in-house specifications. These product are designated:

Az Products meet the NTEP requirements for class III applications.
Bz Products meet the NTEP requirements for class IIIL applications.
Cz Products meet the OIML requirements for class III and IIII applications.
CC/D3 These are arbitrary in-house classifications for products used in non-trade applications.
Note "z" represents the number of divisions (x1000), i.e. A3, B10, C6, etc.

Most weighing systems use load cells where their working or measuring range is well below their rated capacity. In these situations, the values for the load cell *utilization* and *minimum verification interval* (vmin) are important.

The minimum verification interval is defined as the smallest value of a quantity (mass) which may be applied to a load cell without exceeding the maximum permissible error. It is specified as Emax/g, where Emax represents the load cell's rated capacity and g represents a value which is specified by the load cell supplier.

The minimum measuring range can apply over any part of the measuring range between the minimum dead load (Emin) and the rated capacity (Emax).

A load cell may be used over a working range larger that its minimum utilization.

The terms above the central horizontal line are fixed by the design of the load cell, while the terms below are fixed on the conditions of use and cell performance.

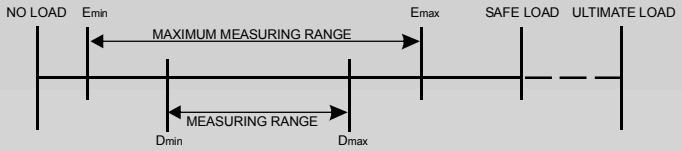


FIG 8 Graphic Relationship of Load Related Terms

0) Approved systems

Legal for trade weighing systems require load cells which are certified according to the National Type Evaluation Program (NTEP) or OIML recommendation R60 (Europe). The requirements in terms of load cell accuracy for the above mentioned systems are:

1) Select a cell which is certified according to the appropriate standard, i.e. products designated "Az" for class III applications.

2) For each load cell, the maximum number of load cell intervals shall not be less than the number of verification scale intervals. For example; a 3000 division class III scale requires A3 load cells.

3) The minimum load cell verification interval shall satisfy the condition:

$$v_{min} \leq e*R / \sqrt{N}$$

where e represents the scale verification interval and R represents the reduction ratio of the load transmitting device (hybrid scales).

$$R = \frac{\text{Load acting on the load cell(s)}}{\text{Load acting on the receptor (scale)}}$$

For example:
A fully electronic scale (R=1), with four load cells and a measuring range of 6t divided into 3000 divisions requires load cells with the following vmin:

$$v_{min} \leq (6000/3000)*(1/\sqrt{4}) \rightarrow v_{min} \leq 1kg$$

1.3.2 Non approved systems

The load cell selection for non-approved weighing systems can be based on the specified error percentages which are indicated on our datasheets. In addition, the following table can be used:

Required System Accuracy	Load Cell	Accuracy
	1	2
Low accuracy "0.5 6 "5%	CC	CC
Medium accuracy "0.1 6 "0.5%	CC/C1	C2
High accuracy "0.02 6"0.1%	C2/C3	C3/C4

1 Standard systems
2 Systems with a large dead load in relation to the measuring range, or systems which are exposed to large temperature changes

1.4 ENVIRONMENTAL PROTECTION

No area of load cell operation causes more confusion and contention than that of environmental protection and sealing standards. Although our industries have in-depth standards and test procedures to define load cell and weighing system performance, no standards have been developed to cover product suitability for specific environmental conditions. In the absence of such standards, most manufacturers have adopted the International Protection system (IP/IEC 529 or EN 40.050) or National Electrical Manufacturers Association Standards (NEMA publication 250). Define the level of sealing for their products. Both standards are good test procedures for environmental sealing when applied to the products for which they were intended - those being electrical enclosures, but they are not very well suited to load cells.

1.4.1 IP Classification

The IP standard describes a system for classifying the degree of protection provided by the enclosures of electrical equipment:

Protection of persons against access to hazardous parts inside the enclosure.
Protection of the equipment inside the enclosure against the ingress of solid foreign objects.
Protection of equipment inside the enclosure against harmful effects due to the ingress of water.

Unfortunately, no definition is given for the term "harmful effects". Presumably, for enclosures, the main problem with water could be one of electrical shock to persons in contact with the enclosure, rather than malfunctioning of the unit. Furthermore, the standard only relates to water ingress and ignores moisture, chemicals, corrosion, etc.

The commonly used categories to describe load cell sealing are:

Ip65 Protected against low pressure jets of water from all directions, limited entrance allowed

Ip66 Protected against strong jets of water e.g. for use on ship decks, limited entrance allowed

Ip67 Protected against the effects of immersion between 15cm and 1m

Ip68 Protected against long periods of immersion under pressure

1.4.2 NEMA Classification

Classifications in the NEMA system run from NEMA 1 to NEMA 12, but load cell manufacturers concern themselves with NEMA 4 and NEMA 6. Unlike the IP system, NEMA does concern itself with environmental conditions such as corrosion, rust, freezing, oil and coolants.

NEMA 4 enclosures are intended for indoor and outdoor use, providing a degree of protection against windblown dust, rain, splashing water, and hose directed water. However, no consideration is given for the effects of internal condensation. Nema 4X enclosures meet the same standards as NEMA 4 and are constructed of 304 stainless steel or other material offering equal corrosion resistance.

NEMA 6 enclosures are used where there is a chance of temporary immersion. This standard calls for the highest part of the enclosure to remain submerged in water, with its highest point 1.83 meters below the surface for 30 minutes. NEMA 6P enclosures are used where prolonged immersion may occur and resistance to corrosion is needed.

While it may seem that NEMA standards offer some advantages over the IP system for corrosion resistance, they only relate to external corrosion of enclosures. This is very limited when applied to the more complex load cell construction and the different effects of corrosion or water ingress.

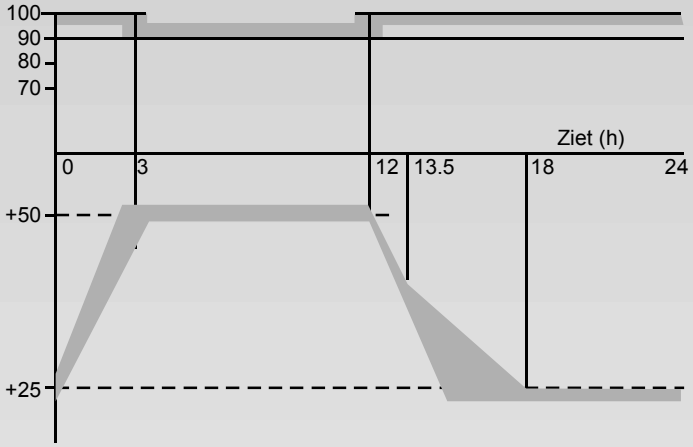
1.4.3 Damp Heat Cycling (IEC 68-2-30)

The IP and NEMA standards don't deal with internal condensation or moisture within the enclosure. However, moisture or condensation is of vital importance in correct load cell operation.

Moisture may enter the inside of the load cell over a long period and have a catastrophic effect, especially when acids or alkalies are present. One test used to determine a load cells ability to withstand moisture or condensation is the Damp Heat Cycling Test. The

object of the IEC standard is "To determine the suitability of components, equipment, or other articles for use and storage under conditions of high humidity when combined with cyclical temperature changes".

It is obvious that this standard is a much more useful classification than the IP or NEMA rating when it comes to defining load cell environmental suitability.



1.4.4 Load cell construction

Besides a given IP-rating or NEMA-classification load cells should also be classified according to their design in terms of cable entry, material of construction and gages sealing method.

Whilst it is relatively common to weld-seal critical areas on a load cell body, one potential problem area is the cable entry. A variety of methods are used to make sure cells are properly sealed at this area.

In most load cells the main cable enters through a conventional cable gland directly into the gage area. Regardless of how well the gage area is sealed, moisture and solvents can penetrate either around the gland or through the center of the cable itself. Often, temperature changes cause a pumping action to occur, pushing moisture down the inside of the cable. Entry also can be via a leaking junction box or through a damaged part of the cable. This can take some time to reach critical areas, but once there it will become sealed in place and do critical damage.

An improvement on the basic cable gland is a water block at the point of cable entry. Here, the main cable terminates at for example a small circuit board with on-going wires leading to the gage area. The block is fully potted to prevent moisture or other contaminants from reaching the critical areas.

The best solution is the use of a glass-to-metal cable entrance. This prevents any contamination from

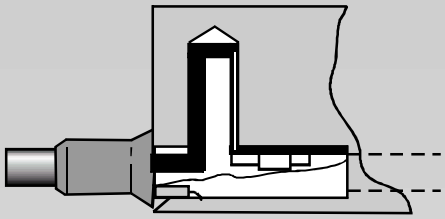


FIG 10 Water Blocked Cable Entry

reaching the gage or other critical areas. In addition, the manufacturing process used must keep the load cell free from residue contaminations. The problem of residuals is usually solved by purging the internal cavity with helium. Revere Transducers model RLC is first filled with helium, which allows leaks to be found with conventional leak detection equipment and just before closing the load cell the helium will be replace by argon.

1.4.5 Corrosion

The corrosion resistance of load cells is a very complex subject, one that is further complicated by the variety of available configurations. As a result it is only possible to use standard corrosion charts as a guidance for load cells. In addition, the following factors must be considered:

Surface finish
Weld areas around seals, bellows and cups
Thickness of seals
Varying construction materials
High stress levels at loading points
Cable material (PVC. PUR or Teflon)

The environment itself plays an important role in how a particular load cell type behaves in practice. Salt water, for example, has different corrosion effects depending on the local circumstances. Stainless steel in stagnant salt water is subject to crevice corrosion and a regular wash down is necessary to avoid degradation.

Unfortunately the term stainless steel has become synonymous with "no corrosion, no problem and no maintenance". While stainless steel load cells usually offer optimum protection in most environments, other factors should be taken into account. In certain applications, painted or plated load cells may offer better long-term protection.

An alternative is wrap-around protective covers. These can provide good environmental protection, but can be self-destructive if corrosive material is trapped inside the cover.

1.5 SUMMARY

Selecting the wrong load cell for an application in terms of environmental compatibility can have far reaching consequences in terms of costs, safety and product reputation. Current classifications fall well short of defining adequate environmental standards for load cells.

The users should compare like-for-like features when selecting products from different manufacturers. If in doubt, they should ask pertinent questions relating to:

Construction of the load cell
Cable entry method
Past experiences

For applications in harsh environments, additional protection for the load cells may be needed to assure their reasonable working life. This can be achieved with enhanced scale designs and the use of additional coatings on the load cell, such as paints, greases and plating. The scale or system design should minimize the possibility of material build-up around the cells. If appropriate, the design should also provide mechanical protection from the effects of direct water and solvents whilst cleaning. Sealing compounds and rubbers used on some load cells can deteriorate when exposed to chemicals or direct sunlight. Because they embrittle rubber, chlorine-based compounds are a particular problem.

2. INSTALLATION

The installation of load cells into a practical field application requires careful attention if the system is to be safe and accurate.

It is a common misconception that a load cell can be considered as a solid piece of metal on which hoppers or platforms can be supported. The performance of a load cell depends primarily on its ability to deflect repeatably under conditions when load is applied or removed. Furthermore, if more than one load cell is used then the deflection and output of each individual cell should be similar on each load point.

To satisfy the above requirements, load cells are mainly used in conjunction with special mounting systems rather then being mounted rigidly between platform/hopper and foundation. Load cell supports should be designed to avoid the following effects to the load cell:

Lateral forces
Bending moments
Torsion moments
Off center loading to the cell
Vibration to the load cell

These effects not only compromise the performance of the load cell, but they can also lead to permanent damage.

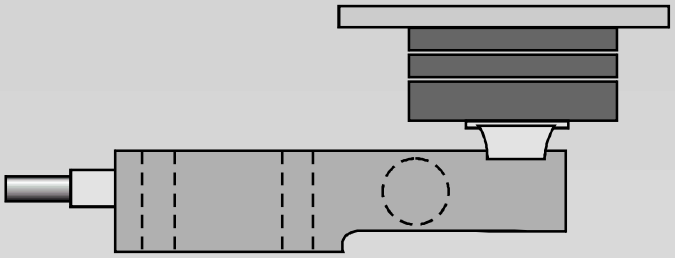


Fig.11 Neoprene anti-vibration pad.Fig.11 Neoprene anti-vibration pad.

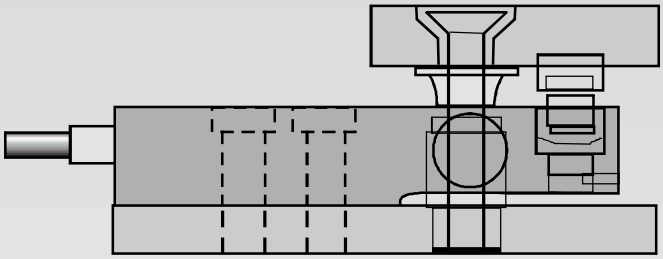


FIG 12 Self Aligning Mount, Based On A Rocker Pin Load Introduction. The Top Plate Is Held Captive To Provide Lift-off Protection and to Restrict The Horizontal Movement.

If major load movement is anticipated, stay rods should be used to restrain a platform (weighbridge) or vessel. Stay rods are installed horizontally and should not transfer any forces to the vessel or scale in the vertical direction, while having sufficient strength in the horizontal direction to be able to absorb side forces. The length of the rods should be chosen as long as possible, as this has a favorable effect on reducing vertical forces.

The arrangement of the stay rods depends on the plan view geometry of the structure. In most cases four rods give the best results.
Stay rods provide stability and accuracy, specially for systems with agitators. They should be installed carefully (exactly horizontal) and without any stress.

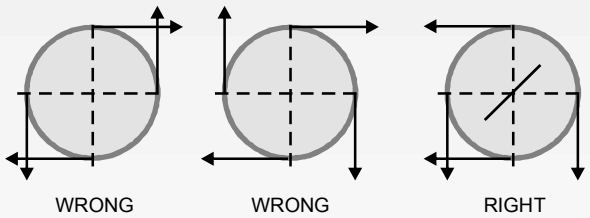


FIG 13 Placing Rods As Indicated In The Drawing Will Cause High Stress In The Stay Rods Or Rotation Of The Vessel.

Stay rods should not be confused with safety rods, which are installed similar, but provide a different function. Safety rods are left loose during normal operation. The are an extra safety feature in the event of wind forces, seismic activity or mechanical failure of mounts or load cells.

Safety rods are strongly recommended for those systems where one of the above events could seriously affect personnel safety or where one of the above events could lead to extensive damage.

In order to assure performance, load cells should be placed on exactly the same horizontal level. Never use mounting bolts to pull uneven surfaces together; shim plates should be used as appropriate.

The preferred orientation of the load cell depends primarily on its design. The load should always be transmitted vertically through the load cell in the way which it was designed to measure force.

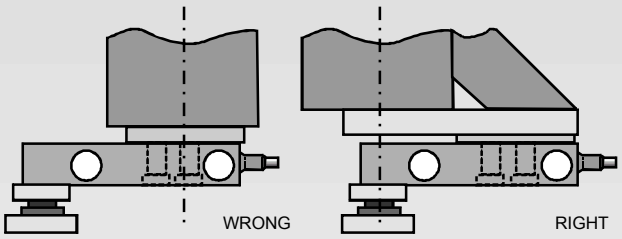


FIG 14 Load Transmission

S-type load cells should be mounted in such a way that side forces are reduced to a minimum; they should never be mounted rigidly (even only at one side) between the structure and hopper. The load cell must be orientated in such a way that the cable entry does not affect weighing accuracy.

In terms of safety, attention should be paid to use the full length of thread, while considerations should be made to provide an external back up system.

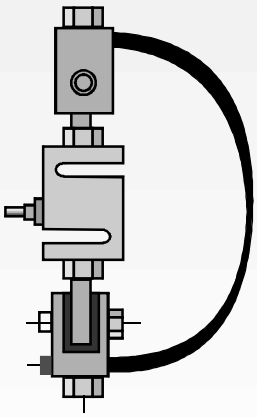


FIG 15 Correct Installation Of S-Type Load Cells

To prevent load cells from being damaged during installation, it is strongly recommended t o use dummies or mounting assemblies that can be "locked". Load cells should be handled with care, especially those with a low rated capacity or with metal bellows construction. Single ended beam load cells are subjected to a momentum and require high quality bolts for safe operation. The amount of torque on these bolts is specified and should be met to achieve the maximum performance.

2.1 Load cell cables

Special attention should be paid in preventing the load cell cable from being damaged during and after installation. Never carry load cells at their cables and provide dripping loops to
prevent water from running directly into the cable entry. Load cells are produced with a four- or six-wire cable. A four-wire cable is calibrated and temperature compensated with a certain length of cable. The performance of the load cell, in terms of temperature stability, will be compromised if the cable is cut; never cut a four-wire load cell cable!

A six-wire load cell cable has two additional wires which can be used to actually measure the excitation voltage at the load cell in order to feed this information back to the indicator. A six-wire load cell is not part of the load cell's temperature compensating system and can be cut to any desired length. However, it should be recognized that the parallel connection of multiple six-wire load cells results in an equal potential difference over all cells. All load cell cables should therefor be shortened to the same length.

2.2 Junction boxes

The junction box is an essential part of the system and should be protected to at least IP65 or NEMA 4. Select the location of the junction box based on the

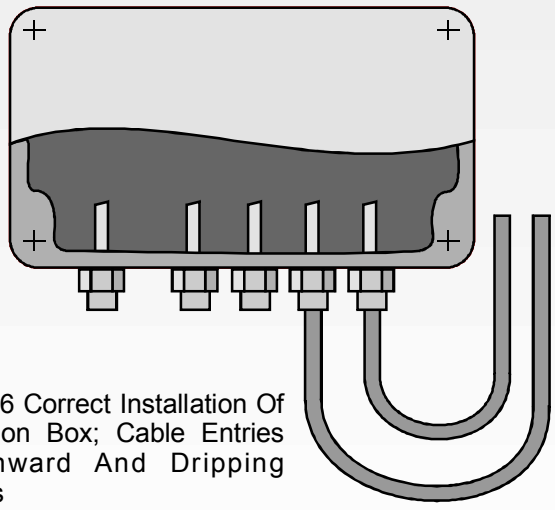


FIG 16 Correct Installation Of Junction Box; Cable Entries Downward And Dripping Loops

environmental conditions; NOT on the ease of installation.

During the installation ensure that no moisture enters the load cell cable before and during installation. A bag of drying agent (silica gel) may be enclosed to absorb moisture. However, the drying agent should never make contact with any non-insulated wiring in the box.

Use junction boxes with high quality terminals or use solder connections. The components used for corner correction should be absolutely temperature stable.

2.3 Welding

Avoid electric welding after installation of the load cells. If welding is necessary and the load cells can not be removed then disconnect each individual load cell cable from the junction box or measuring device.

Place the clamp earthing electrode of the welding apparatus in the close proximity of the weld to avoid a current path through the load cells. Furthermore, connect a flexible copper lead over each load cell.

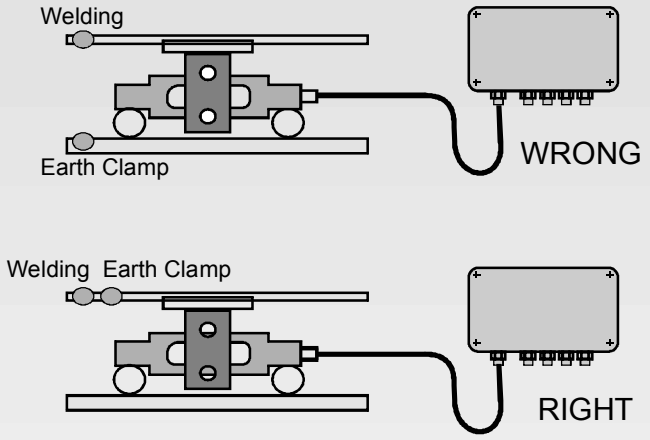


FIG 17 Electrical welding after installation of the Load Cells.

2.4 Lightning protection

Modern weighing systems rely heavily on high performance electronic components, but the features that make this possible also makes these components more vulnerable to the disruption and damage that can be caused by lightning or over voltage in general.

Investigations indicate that a lightning strike within a 900ft radius of the geometrical center of the site will definitely have a detrimental effect on the weighbridge. Nor is such damage confined only to earth strikes, since cloud-to-cloud strikes are equally capable of producing an electromagnetic pulse (EMP) of sufficient strength to cause damage.

In most cases, the actual load cell damage is a direct result of a potential difference, well in excess of 1000 volts, between circuit and housing.

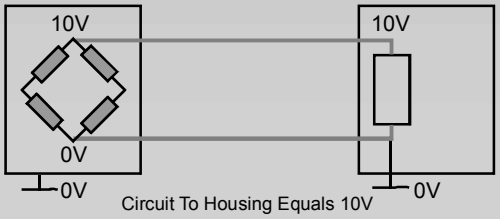


FIG 18 Load Cell and Indicator are both connected to ground at a considerable distance from each other.

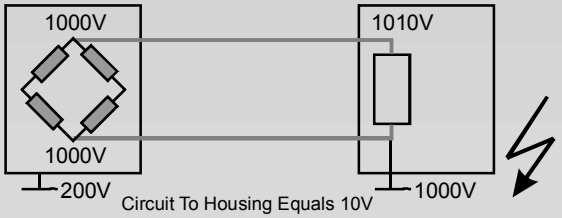


FIG 19 The potential at the earthing points will rise as a direct result of a lightning strike (to earth). However, +both points will not rise to the same potential because of the ground resistance. Although the excitation voltage remains 10V, the potential difference between circuit and housing increases far above an acceptable value.

It should be recognized that a high potential difference between housing and load cell circuit can be caused by:

A rise of local earth potential when a lightning strike is dissipated through the ground.
Severe over-voltages or electromagnetic pulses via the main power supply.

The damage in both cases might result in a complete burn out of the component, but this is not always true. It is possible that only a part of the load cells circuit or one of the strain gage's glue layer is damaged. As a result the scale starts to drift and/or will not hold its return to zero. Sometimes these problems appear weeks after the actual lightning strike!

It is obvious that a high level of protection against lightning strikes can only be established if the complete system is protected. The decision to protect a system or part of a system should be based on: the location (urban area or open field), the average ground flash density (ask for statistics at the appropriate institute), the costs incurred during a breakdown period, the expenses for the replacement of parts and workmanship, and the insurance company requirements (or premiums!).

Protection can be considered in two stages; external and internal.

2.4.1 External protection

External protection entails bonding the steel roof of the cabin where the indicator is located or any nearby structure or a high protection mast in such a matter as to

provide a preferential point of discharge and safely conduct the surge to earth via conductors.

In fact considerable controversy surrounds such external protection. A weighbridge or in general a scale is not an attractive point for lightning to strike, but a 60ft mast has an attractive radius of 240ft. Lightning which might otherwise have struck a building or tree 180ft or more away will now be captured to produce a current surge to ground within the very neighborhood of the weighbridge!

Unless very stringent precautions are taken such a surge will produce an electromagnetic induced pulse which will undoubtedly cause severe damage to the weighbridge.

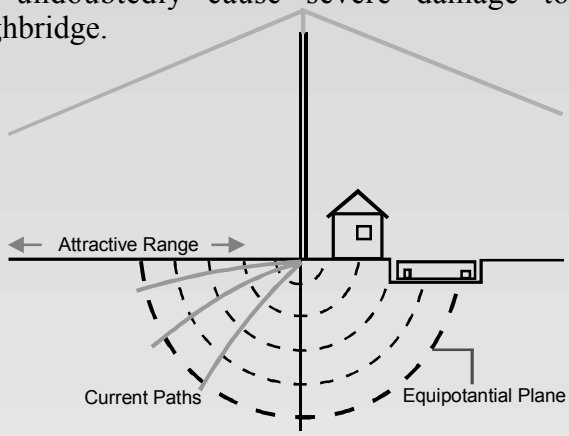


FIG 20 External Lightning Protection.

2.4.2 Internal protection

Internal lightning protection sets out to provide potential equalization throughout the whole system by defining a central point about which all the electrical systems can float or by using Surge Protection Devices (SPDs).

Surge protection devices are designed to control line-line and line-earth voltages to levels acceptable to the equipment. An SPD incorporates combinations of gas-filled discharge tubes for high current surge diversion and zanier diodes for secure voltage clamping with minimal leakage. For ac power applications, varistors are often used because of their higher power absorption capability. Most SPDs are connected in series, similar to shunt diode barriers for intrinsically safe systems.

Any device which works by diverting large currents to a local ground must have a low impedance connection to that ground. This means that the bonding connection must be of low resistance (well below 0,5W), short in length and as direct as possible without sharp bends. Verify the earth connections at least twice a year and coat all connections with a good antioxidant grease.

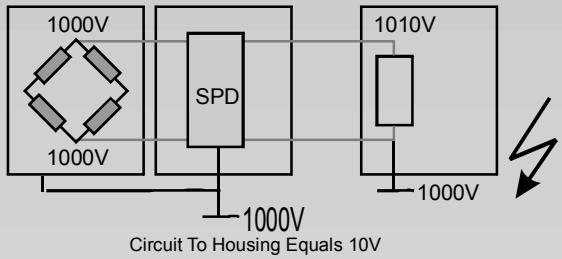
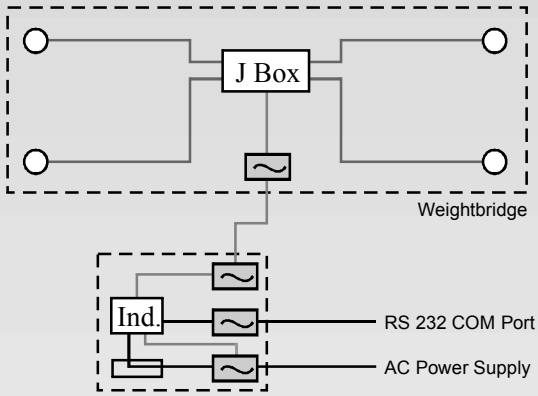


FIG 21 Systems with unavoidable multiple points of earthing should use an SPD to divert surges to a local ground. By doing so, the whole system will rise and fall at the same potential.

Any external connection such as ac power lines, communication ports and the signal/excitation cable is a potential source of surges or transients. Central to the provision of lightning protection is therefore the installation of an SPD at all external connections:



3. MAINTENANCE

Maintenance is often overlooked or ignored by both load cell users and service companies. However, the regular service and maintenance of load cells in a weighing system will greatly improve their long-term reliability and performance as well as greatly reduce their sensitivity to corrosion. Maintenance inspections can be divided into two categories:

 # Routine:

Performed at periodic intervals, it includes the removal of any material or debris buildup from around the load cells and mounting fixtures. Serious damage can occur to the load cells if mounting systems do not function correctly. Any damage or degradation of surface coatings should be remedied and all cables and junction-boxes should be checked. To minimize the effects of flooding, any drainage systems in the pit should be free from debris. Where required, regular wash down of the load cell should be carried out to prevent chemical attack.

 # Ad hoc:

Made immediately after any adverse or unexpected events such as flash floods, gales, seismic activity or

electrical storms. In General; careful consideration must be given to any reason for failure. If this has occurred as a result of ingress of water or chemicals, then continued deterioration of any other load cell(s) in the system can be expected, resulting in mechanical failure. This failure can have serious safety and cost consequences.

Always remove the load cell with care and attach a label with comments to the problem or mode of failure. Never cut the cable at the gland to facilitate removal; load cells cannot be tested without cables!

DO'S & DON'TS OF LOAD CELLS

LOAD CELL SELECTION AND DESIGN

Do select the right load cell for the application in terms of type and environmental compatibility.
Do choose the right capacity.
Do consider the required accuracy class.
Do consider all environmental aspects before making the final choice (whether they are always or occasionally present at the place(s) the load cells will operate).
Do provide for any additional environmental protection at the design stage.
Do design-in adequate over/under load protection as well as protection from other mechanical damage (e.g. physical abuse, rodent problems).

Don't make the choice based only on price - cost of ownership is more important.
Don't allow load cells to operate above their rated capacity.
Don't over specify - look at overall system limitations on accuracy (e.g. mechanical pipe work, vibration etc.).
Don't ignore that hurricane or flood that comes once every 2 or 3 years.
Don't build in water / debris traps.
Don't assume "it" will never happen, and never use the load cell as a mechanical fuse.
Don't forget to provide adequate protection for the load cell cable, near the load cell if possible.

INSTALLATION AND FITTING

Do use dummy load cells prior to installation.
Do store and handle load cells carefully prior to and during installation, and try to keep copies of the Certificate of Calibration in a safe place. Check load cells before fitting for correct model, capacity, thread combination, etc.
Do check that any threaded fittings screw smoothly into the load cell before final assembly.
Do use high quality bolts with the recommended torque.
Do check that adequate and accurately fitted mounting surfaces are provided.
Do use care when tightening mounting bolts and restraints such as tie-bars.
Do use lock nuts appropriate on threaded fittings, especially if vibration is present.
Do check cable color code for load cell prior to connection - Revere Transducers has two basic color codes.

Do use good quality connecting terminals / Junction Boxes. Solder joints if possible.
Don't carry out electric welding near load cells if possible.
Don't forget to check specific storage and operating temperature ranges for the load cells.
Don't ever carry load cells by their cables !
Don't force bolts or other threaded assemblies.
Don't use mounting bolts to pull uneven surfaces together - use shims as appropriate.
Don't use excessive force when fitting / tightening mounting bolts or hardware, especially on low capacity cells.
Don't twist "S" cells when tightening threaded fittings.
Don't cut load cell cables unless necessary, performance may be effected.
Don't allow moisture to get at any interconnections.
Don't allow load cell to be the electrical link between ground and metal weigh structure.

MAINTENANCE

Do regularly inspect load cells and weigh system especially after extreme weather conditions (electrical storms, flooding, seismic activity, etc.) and also before and after the seasons.
Do check for corrosion damage to the load cell and mounting hardware. If practical, carry out cleaning and any remedial work (paint or other protective coating) before it is too late.
Do give special care and attention to critical areas of the load cell such as metal bellows, seals etc. Those features are important in the operation and performance of the product.
Don't allow build up of debris around load cell or mounts.
Don't allow any drains to become blocked with leaves or other debris.
Don't disconnect and just re-calibrate one or more load cells in a system if they cease to function. Mechanical failure may have catastrophic effects.